

UAF 42 (UAF 41) Variable-mu diode-pentode

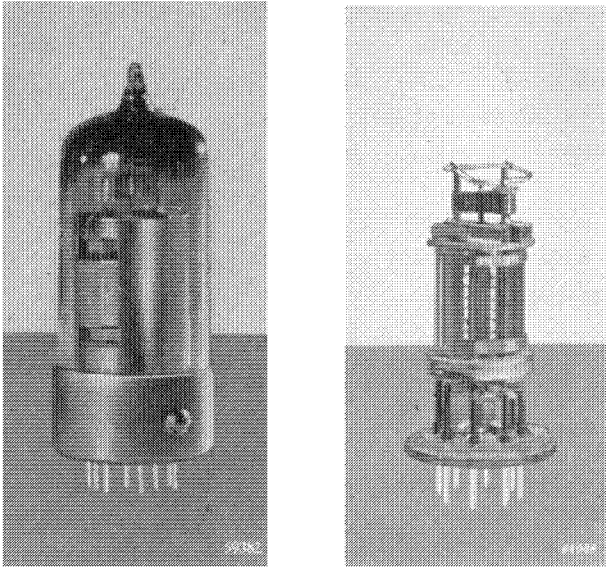


Fig. 1

The UAF 42, showing the electrode system (approximately actual size).

The UAF 42 is a variable-mu diode-pentode for A.C./D.C. receivers having a heater circuit carrying 100 mA. The pentode section is intended for use as R.F., I.F. or A.F. amplifier, the diode section being suitable for detection and A.G.C.

Since the UAF 42 — apart from the heater — is identical with the EAF 42, further particulars will be found in the description of the latter valve.

TECHNICAL DATA OF THE DIODE-PENTODE UAF 41

Heater data

Heating: A.C. or D.C., indirect, series feed

Heater current . . . . .  $I_f$  = 100 mA

Heater voltage . . . . .  $V_f$  = 12.6 V

Capacitances (cold valve)

*Pentode section*

Input capacitance . . . . .  $C_{g1}$  = 4.0 pF

Output capacitance . . . . .  $C_a$  = 6.5 pF

Anode - control grid . . . . .  $C_{ag1}$  < 0.002 pF

Heater - control grid . . . . .  $C_{g1f}$  < 0.05 pF

# UAF 41

## Diode section

Anode - cathode . . . . .	$C_{da}$	=	3.8 pF
Anode - heater . . . . .	$C_{df}$	<	0.02 pF

## Between diode and pentode sections

Diode anode - pentode control grid . . . . .	$C_{dg1}$	<	0.0015 pF
Diode anode - pentode anode	$C_{da}$	<	0.15 pF

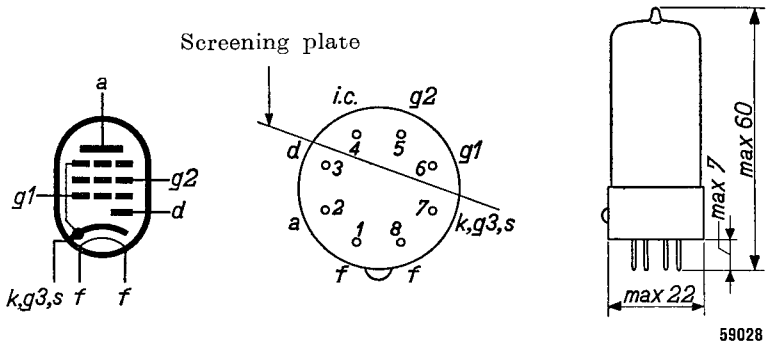


Fig. 2

Electrode arrangement, electrode connections and maximum dimensions in mm of the UAF 41.

## Operating characteristics of the pentode section used as R.F. or I.F. amplifier (see Figs. 6 and 7)

Anode and supply voltage . . . . .	$V_a = V_b =$	100	170	V
Screen grid resistor . . . . .	$R_{g2} =$	44	44	kΩ
Bias resistor . . . . .	$R_k =$	300	300	Ω
Grid bias . . . . .	$V_{g1} =$	$\overline{-1.1 \quad -17}$	$\overline{-2 \quad -28}$	V
Anode current . . . . .	$I_a =$	2.8 —	5 —	mA
Screen grid current . . . . .	$I_{g2} =$	0.9 —	1.6 —	mA
Mutual conductance . . . . .	$S =$	1650 16.5	1800 18	$\mu\text{A/V}$
Internal resistance . . . . .	$R_i =$	1.0 >10	1.2 >10	MΩ
Equivalent noise resistance . . . . .	$R_{eq} =$	7 —	9 —	kΩ
Amplification factor, second grid with respect to first grid . . . . .	$\mu_{g2g1} =$	19 —	19 —	

**Operating characteristics of the pentode section used as resistance-coupled A.F. amplifier** (for circuit see Fig. 5; for microphonic properties of this circuit see description of the EAF 42)

- A. Supply voltage  $V_b=170$  V Anode resistor  $R_a=0.2$  M $\Omega$   
 Bias resistor  $R_k=2.7$  k $\Omega$  Screen grid resistor  $R_{g2}=0.73$  M $\Omega$

Control voltage $-V_R$ (V)	Anode current $I_a$ (mA)	Screen grid current $I_{g2}$ (mA)	Amplification $V_o/V_i$	Distortion (%) at an output voltage of		
				3 $V_{RMS}$	5 $V_{RMS}$	8 $V_{RMS}$
0	0.58	0.18	78	0.8	1.1	1.6
5	0.46	0.13	25	1.2	2.1	4.0
10	0.36	0.08	15	2.0	3.2	4.8
15	0.26	0.05	10	2.6	3.7	5.8
20	0.18	0.03	7	3.0	4.4	7.3
25	0.12	0.01	5	5.1	8.0	13.0

- B. Supply voltage  $V_b=100$  V Anode resistor  $R_a=0.2$  M $\Omega$   
 Bias resistor  $R_k=2.7$  k $\Omega$  Screen grid resistor  $R_{g2}=0.73$  M $\Omega$

Control voltage $-V_R$ (V)	Anode current $I_a$ (mA)	Screen grid current $I_{g2}$ (mA)	Amplification $V_o/V_i$	Distortion (%) at an output voltage of:		
				3 $V_{RMS}$	5 $V_{RMS}$	
0	0.34	0.10	73	0.8	1.0	
2.5	0.26	0.07	27	3.0	4.0	
5.0	0.20	0.05	15	3.5	5.0	
7.5	0.16	0.04	10	3.8	5.7	
10.0	0.12	0.02	7	4.4	7.5	
12.5	0.08	0.01	5.5	5.7	9.0	

**Operating characteristics of the pentode section used as resistance-coupled A.F. triode** (screen grid connected to anode)

- A. Supply voltage  $V_b=170$  V Anode resistor  $R_a=0.1$  M $\Omega$   
 Bias resistor  $R_k=1.2$  k $\Omega$

Control voltage $-V_R$ (V)	Anode current $I_a$ (mA)	Amplification $V_o/V_i$	Distortion (%) at an output voltage of		
			3 $V_{RMS}$	5 $V_{RMS}$	8 $V_{RMS}$
0	1.3	15	1.2	1.8	3.4
5	0.9	7.3	1.5	2.4	3.8
10	0.6	5.0	1.3	2.1	3.0
15	0.4	3.7	1.9	3.7	6.0
20	0.2	2.6	4.0	6.8	9.5

# UAF 41

B. Supply voltage  $V_b=100$  V Anode resistor  $R_a=0.1$  M $\Omega$   
 Bias resistor  $R_k=2.3$  k $\Omega$

Control voltage — $V_R$ (V)	Anode current $I_a$ (mA)	Amplification $V_o/V_i$	Distortion (%) at an output voltage of		
			3 $V_{RMS}$	5 $V_{RMS}$	
0	0.55	12	1.9	2.8	
2.5	0.45	7.2	2.6	5.6	
5.0	0.30	4.9	2.3	4.9	
7.5	0.20	3.8	3.0	6.0	
10	0.15	2.8	6.0	10.0	

## Limiting values of the pentode section

Anode voltage, valve biased to cut-off . . . . .	$V_{a_0}$	= max.	550 V
Anode voltage . . . . .	$V_a$	= max.	250 V
Anode dissipation . . . . .	$W_a$	= max.	2 W
Screen grid voltage, valve biased to cut-off . . . . .	$V_{g2_0}$	= max.	550 V
Screen grid voltage, valve controlled . . . . .	$V_{g2}(I_a < 3 \text{ mA})$	= max.	250 V
Screen grid voltage, valve not controlled . . . . .	$V_{g2}(I_a = 6 \text{ mA})$	= max.	150 V
Screen grid dissipation . . . . .	$W_{g2}$	= max.	0.3 W
Cathode current . . . . .	$I_k$	= max.	10 mA
Grid current starting point . . . . .	$V_{g1}(I_{g1} = +0.3 \mu\text{A})$	= max.	-1.3 V
External resistance between first grid and cathode . . . . .	$R_{g1}$	= max.	3 M $\Omega$
External resistance between heater and cathode . . . . .	$R_{fk}$	= max.	20 k $\Omega$
Voltage between heater and cathode . . . . .	$V_{fk}$	= max.	150 V

## Limiting values of the diode section

Peak anode inverse voltage . . . . .	$V_{d \text{ inv } p}$	= max.	350 V
Diode current . . . . .	$I_d$	= max.	0.8 mA
Peak diode current . . . . .	$I_{dp}$	= max.	5 mA
Diode current starting point . . . . .	$V_d(I_d = +0.3 \mu\text{A})$	= max.	-1.3 V
External resistance between heater and cathode . . . . .	$R_{fk}$	= max.	20 k $\Omega$
Voltage between heater and cathode . . . . .	$V_{fk}$	= max.	150 V

**TECHNICAL DATA OF THE DIODE-PENTODE UAF 42**

**Heater data**

Heating: indirect, A.C. or D.C., series feed

Heater current . . . . .	$I_f$	=	100 mA
Heater voltage . . . . .	$V_f$	=	12.6 V

**Capacitances (cold valve)**

*Pentode section*

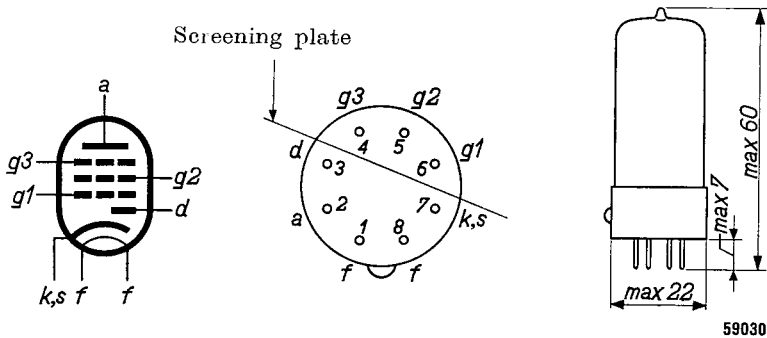
Input capacitance . . . . .	$C_{g1}$	=	4.1 pF
Output capacitance . . . . .	$C_a$	=	5.2 pF
Anode - control grid . . . . .	$C_{ag1}$	<	0.002 pF
Heater - control grid . . . . .	$C_{gf}$	<	0.05 pF

*Diode section*

Anode - cathode . . . . .	$C_a$	=	3.3 pF
Anode - heater . . . . .	$C_{af}$	<	0.02 pF

*Between diode and pentode sections*

Diode anode - pentode control grid . . . . .	$C_{ag1}$	<	0.0015 pF
Diode anode - pentode anode . . . . .	$C_{aa}$	<	0.15 pF



**Fig. 3**

Electrode arrangement, electrode connections and maximum dimensions in mm of the UAF 42.

# UAF 42

## Operating characteristics of the pentode section used as R.F. or I.F. amplifier (see Figs. 8 to 11 incl.)

Anode and supply voltage . . . . .	$V_a = V_b =$	100	170	V
Voltage on third grid . . . . .	$V_{g3} =$	0	0	V
Screen grid resistor . . . . .	$R_{g2} =$	56	56	k $\Omega$
Bias resistor . . . . .	$R_k =$	310	310	$\Omega$
Grid bias . . . . .	$R_{g1} =$	-1.2 -16	-2 -28	V
Screen grid voltage . . . . .	$V_{g2} =$	50 —	85 —	V
Anode current . . . . .	$I_a =$	2.8 —	5 —	mA
Screen grid current . . . . .	$I_{g2} =$	0.9 —	1.5 —	mA
Mutual conductance . . . . .	$S =$	1700 17	2000 20	$\mu\text{A/V}$
Internal resistance . . . . .	$R_i =$	0.85 >10	0.9 >10	M $\Omega$
Equivalent noise resistance . . . . .	$R_{eq} =$	5.8 —	7.5 —	k $\Omega$
Amplification factor, second grid with respect to first grid . . . . .	$\mu_{g2g1} =$	16 —	16 —	

Anode and supply voltage . . . . .	$V_a = V_b =$	200	V
Voltage on third grid . . . . .	$V_{g3} =$	0	V
Screen grid resistor . . . . .	$R_{g2} =$	76	k $\Omega$
Bias resistor . . . . .	$R_k =$	310	$\Omega$
Grid bias . . . . .	$V_{g1} =$	-2 -34	V
Screen grid voltage . . . . .	$V_{g2} =$	85 —	V
Anode current . . . . .	$I_a =$	5 —	mA
Screen grid current . . . . .	$I_{g2} =$	1.5 —	mA
Mutual conductance . . . . .	$S =$	2000 20	$\mu\text{A/V}$
Internal resistance . . . . .	$R_i =$	1.0 >10	M $\Omega$
Equivalent noise resistance . . . . .	$R_{eq} =$	7.5 —	k $\Omega$
Amplification factor, second grid with respect to first grid . . . . .	$\mu_{g2g1} =$	16	—

## Operating characteristics of the pentode section used as R.F. or I.F. amplifier (Screen grid voltage obtained by means of the same potentiometer as that of the UCH 41, for circuit diagram see Fig. 4 ; see also Figs. 15, 16 and 17)

Anode and supply voltage . . . . .	$V_a = V_b =$	100	170	V
Voltage on third grid . . . . .	$V_{g3} =$	0	0	V
Resistor between supply voltage and screen grids . . . . .	$R_1 =$	12	12	k $\Omega$
Resistor between screen grids and chassis . . . . .	$R_2 =$	27	27	k $\Omega$
Bias resistor . . . . .	$R_k =$	250	250	$\Omega$
Grid bias . . . . .	$V_{g1} =$	-1.0 -10.5	-1.8 -18	V
Screen grid voltage . . . . .	$V_{g2} =$	53 69	87 117	V
Anode current . . . . .	$I_a =$	3.0 —	5.5 —	mA
Screen grid current . . . . .	$I_{g2} =$	1.0 —	1.7 —	mA
Mutual conductance . . . . .	$S =$	1850 18	2100 21	$\mu\text{A/V}$
Internal resistance . . . . .	$R_i =$	0.75 >10	0.8 >10	M $\Omega$
Equivalent noise resistance . . . . .	$R_{eq} =$	6 —	8 —	k $\Omega$
Amplification factor, second grid with respect to first grid . . . . .	$\mu_{g2g1} =$	16 —	16 —	

**Operating characteristics of the pentode section used as R.F. or I.F. amplifier;** screen grid voltages of UAF 42 and UCH 42 obtained by means of a common potentiometer (see Figs. 18, 19 and 20)

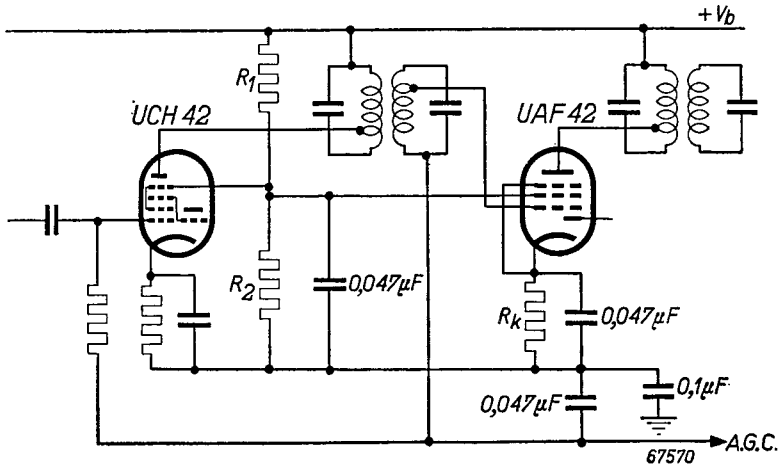
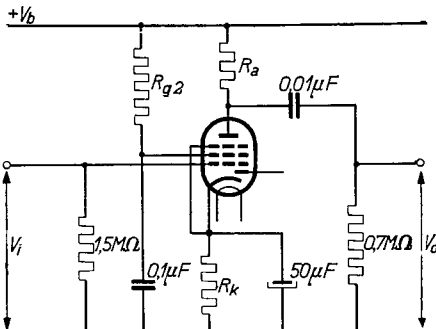


Fig. 4

Anode and supply voltage . . . . .	$V_a = V_b =$	100	170	V
Voltage on third grid . . . . .	$V_{g3} =$	0	0	V
Resistor between supply voltage and screen grids . . . . .	$R_1 =$	15	15	kΩ
Resistor between screen grids and chassis . . . . .	$R_2 =$	22	22	kΩ
Bias resistor . . . . .	$R_k =$	330	330	Ω
Grid bias . . . . .	$V_{g1}$	= -1.0 - 9.5		-1.8 - 15.5 V
Screen grid voltage . . . . .	$V_{g2}$	= 43	58	70 99 V
Anode current . . . . .	$I_a$	= 2.3	—	4.0 — mA
Screen grid current . . . . .	$I_{g2}$	= 0.65	—	1.1 — mA
Mutual conductance . . . . .	$S$	= 1500	15	1750 17.5 μA/V
Internal resistance . . . . .	$R_i$	= 0.95	>10	0.95 >10 MΩ
Equivalent noise resistance . . . . .	$R_{eq}$	= 6.1	—	7.8 — kΩ
Amplification factor, second grid with respect to first grid . . . . .	$\mu_{g2g1}$	= 16	—	16 —



**Operating characteristics of the pentode section used as resistance-coupled A.F. amplifier (for particulars concerning microphony, see description of the EAF 42)**

# UAF 42

A. Supply voltage  $V_b=170$  V Anode resistor  $R_a=0.22$  M $\Omega$   
 Bias resistor  $R_k=2.7$  k $\Omega$  Screen grid resistor  $R_{g2}=0.82$  M $\Omega$

Control voltage $-V_R$ (V)	Anode current $I_a$ (mA)	Screen grid current $I_{g2}$ (mA)	Amplification $V_o/V_i$	Distortion (%) at an output voltage of		
				3V <sub>RMS</sub>	5V <sub>RMS</sub>	8V <sub>RMS</sub>
0	0.50	0.17	80	0.8	1.0	1.2
5	0.38	0.12	23	1.5	2.5	4.0
10	0.28	0.09	14	1.9	3.2	5.0
15	0.20	0.06	9	2.6	4.2	6.5
20	0.14	0.04	6	3.6	6.0	9.0

B. Supply voltage  $V_b=170$  V Anode resistor  $R_a=0.1$  M $\Omega$   
 Bias resistor  $R_k=1.5$  k $\Omega$  Screen grid resistor  $R_{g2}=0.33$  M $\Omega$

Control voltage $-V_R$ (V)	Anode current $I_a$ (mA)	Screen grid current $I_{g2}$ (mA)	Amplification $V_o/V_i$	Distortion (%) at an output voltage of		
				3 V <sub>RMS</sub>	5 V <sub>RMS</sub>	8 V <sub>RMS</sub>
0	1.05	0.37	68	0.75	0.8	1.1
5	0.71	0.25	20	2.2	3.2	5.0
10	0.48	0.17	10	2.4	3.7	5.5
15	0.30	0.11	6	3.0	4.5	7.0
20	0.16	0.07	3.5	5.2	8.0	12

C. Supply voltage  $V_b=100$  V Anode resistor  $R_a=0.22$  M $\Omega$   
 Bias resistor  $R_k=2.7$  k $\Omega$  Screen grid resistor  $R_{g2}=0.82$  M $\Omega$

Control voltage $-V_R$ (V)	Anode current $I_a$ (mA)	Screen grid current $I_{g2}$ (mA)	Amplification $V_o/V_i$	Distortion (%) at an output voltage of	
				3 V <sub>RMS</sub>	5 V <sub>RMS</sub>
0	0.29	0.09	75	0.9	1.1
2.5	0.22	0.07	27	2.6	4.4
5.0	0.17	0.05	15	3.2	5.0
7.5	0.13	0.04	10	4.0	6.5
10	0.10	0.03	7	5.2	8.0

D. Supply voltage  $V_b=100$  V Anode resistor  $R_a=0.1$  M $\Omega$   
 Bias resistor  $R_k=1.5$  k $\Omega$  Screen grid resistor  $R_{g2}=0.33$  M $\Omega$

Control voltage $-V_R$ (V)	Anode current $I_a$ (mA)	Screen grid current $I_{g2}$ (mA)	Amplification $V_o/V_i$	Distortion (%) at an output voltage of	
				3 V <sub>RMS</sub>	5 V <sub>RMS</sub>
0	0.58	0.21	60	0.9	1.0
2.5	0.43	0.14	25	2.3	4.5
5.0	0.31	0.10	12	3.5	6.0
7.5	0.21	0.07	7.5	4.7	8.0
10	0.14	0.05	5	7.0	11



**Operating characteristics of the pentode section used as resistance-coupled A.F. triode** (screen grid connected to anode)

A. Supply voltage  $V_b=170$  V Anode resistor  $R_a=0.1$  M $\Omega$   
 Bias resistor  $R_k=1.8$  k $\Omega$

Control voltage $-V_R$ (V)	Anode current $I_a$ (mA)	Amplification $V_o/V_i$	Distortion (%) at an output voltage of		
			3 V <sub>RMS</sub>	5 V <sub>RMS</sub>	8 V <sub>RMS</sub>
0	1.20	12	1.4	2.2	3.2
5	0.84	6.5	1.4	2.2	3.7
10	0.58	5.0	1.4	2.3	3.8
15	0.37	3.5	1.7	2.7	4.6
20	0.22	2.5	3.2	5.0	8.0

B. Supply voltage  $V_b=170$  V Anode resistor  $R_a=0.05$  M $\Omega$   
 Bias resistor  $R_k=1.2$  k $\Omega$

Control voltage $-V_R$ (V)	Anode current $I_a$ (mA)	Amplification $V_o/V_i$	Distortion (%) at an output voltage of		
			3 V <sub>RMS</sub>	5 V <sub>RMS</sub>	8 V <sub>RMS</sub>
0	2.05	12	1.3	2.0	2.9
5	1.37	6.5	1.6	2.8	4.6
10	0.92	4.5	1.7	2.9	4.8
15	0.60	3.5	2.6	4.0	6.6
20	0.32	2.2	4.5	7.5	11

C. Supply voltage  $V_b=100$  V Anode resistor  $R_a=0.1$  M $\Omega$   
 Bias resistor  $R_k=1.8$  k $\Omega$

Control voltage $-V_R$ (V)	Anode current $I_a$ (mA)	Amplification $V_o/V_i$	Distortion (%) at an output voltage of	
			3 V <sub>RMS</sub>	5 V <sub>RMS</sub>
0	0.70	12	2.0	2.2
2.5	0.50	7	2.4	4.5
5.0	0.36	5	2.4	4.5
7.5	0.25	4	2.7	4.7
10	0.17	3	4.2	6.6

# UAF 42

D. Supply voltage  $V_b=100$  V Anode resistor  $R_a=0.05$  M $\Omega$   
 Bias resistor  $R_k=1.2$  k $\Omega$

Control voltage $-V_R$ (V)	Anode current $I_a$ (mA)	Amplification $V_o/V_i$	Distortion (%) at an output voltage of	
			3 $V_{RMS}$	5 $V_{RMS}$
0	1.18	12	1.7	2.6
2.5	0.80	7	3.0	5.1
5.0	0.56	5	3.6	5.7
7.5	0.38	3.5	4.2	6.8
10	0.24	2.5	6.5	10

## Limiting values of the pentode section

Anode voltage, cut-off condition . . . . .	$V_{a_o}$	= max.	550 V
Anode voltage . . . . .	$V_a$	= max.	250 V
Anode dissipation . . . . .	$W_a$	= max.	2 W
Screen grid voltage, cut-off condition . . . . .	$V_{g2_o}$	= max.	550 V
Screen grid voltage, valve controlled . . . . .	$V_{g2}(I_a < 2.5 \text{ mA})$	= max.	250 V
Screen grid voltage uncontrolled valve . . . . .	$V_{g2}(I_a = 5 \text{ mA})$	= max.	125 V
Screen grid dissipation . . . . .	$W_{g2}$	= max.	0.3 W
Cathode current . . . . .	$I_k$	= max.	10 mA
Grid current starting point . . . . .	$V_{g1}(I_{g1} = +0.3 \mu\text{A})$	= max.	-1.3 V
External resistance between grid 1 and cathode . . . . .	$R_{g1}$	= max.	3 M $\Omega$
External resistance between grid 3 and cathode . . . . .	$R_{g3}$	= max.	3 M $\Omega$
External resistance between heater and cathode . . . . .	$R_{fk}$	= max.	20 k $\Omega$
Voltage between heater and cathode . . . . .	$V_{fk}$	= max.	150 V

## Limiting values of the diode section

Peak anode inverse voltage . . . . .	$V_{d \text{ inv } p}$	= max.	350 V
Diode current . . . . .	$I_d$	= max.	0.8 mA
Peak diode current . . . . .	$I_{dp}$	= max.	5 mA

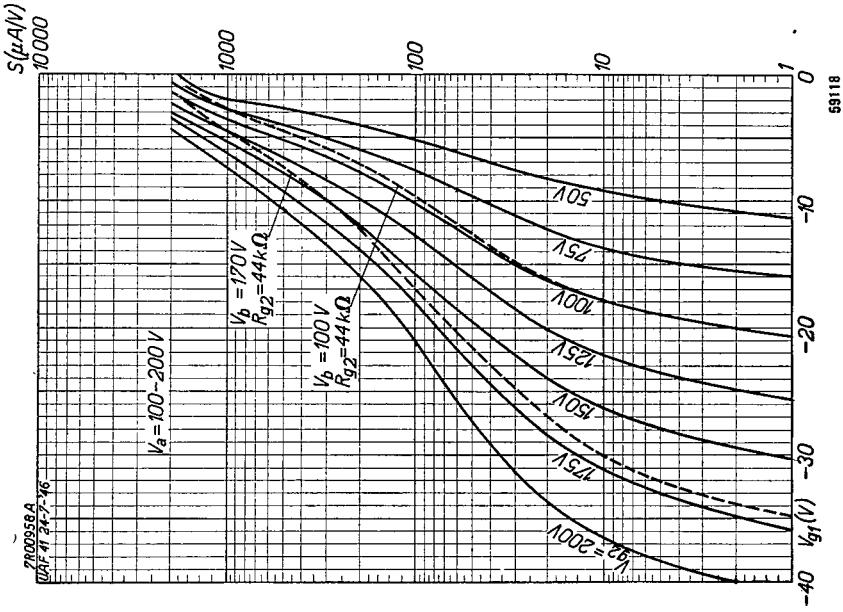


Fig. 7

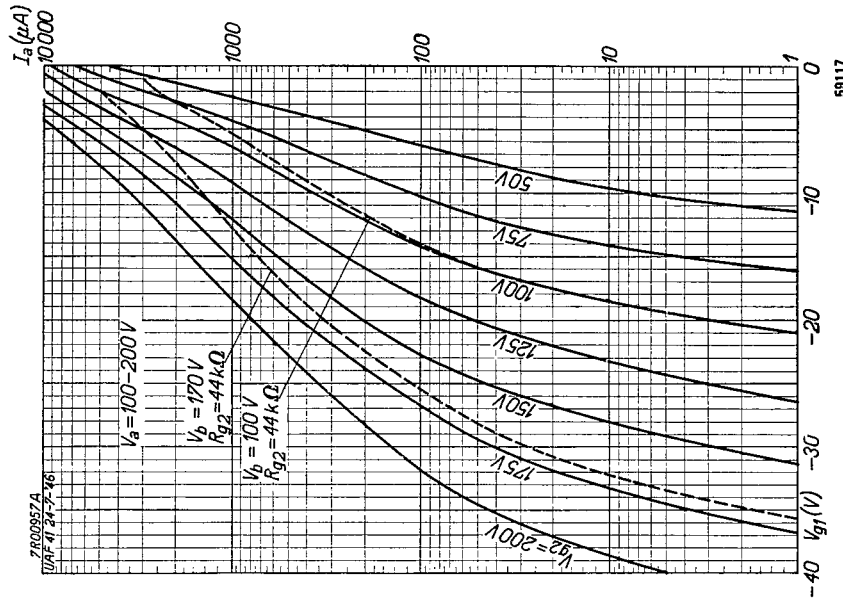


Fig. 6

Anode current ( $I_a$ , Fig. 6) and mutual conductance ( $S$ , Fig. 7) of the UAF 41 as functions of the grid bias  $V_{g1}$  for different values of the screen grid voltage ( $V_{g2}$ ). The dotted lines indicate the variations in anode current and mutual conductance when a series resistor  $R_{g2}$  of 44 kΩ is included in the screen grid circuit.

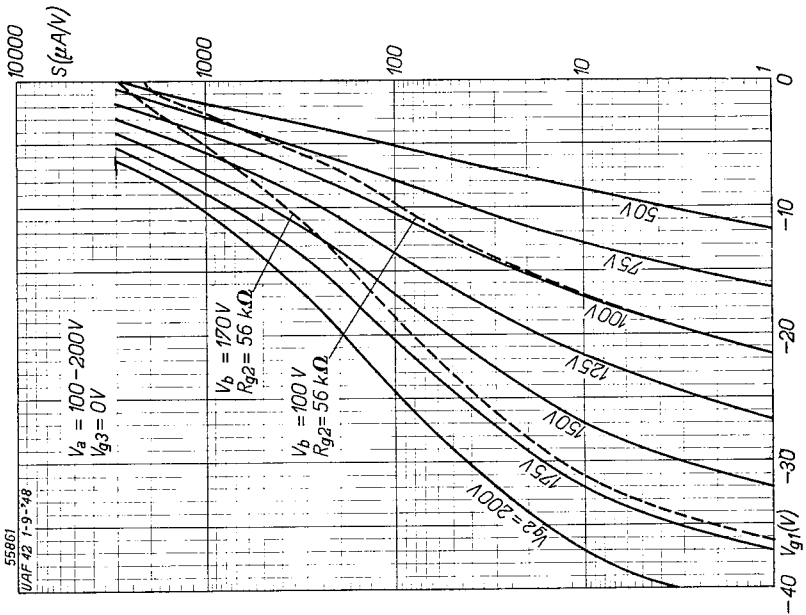


Fig. 9

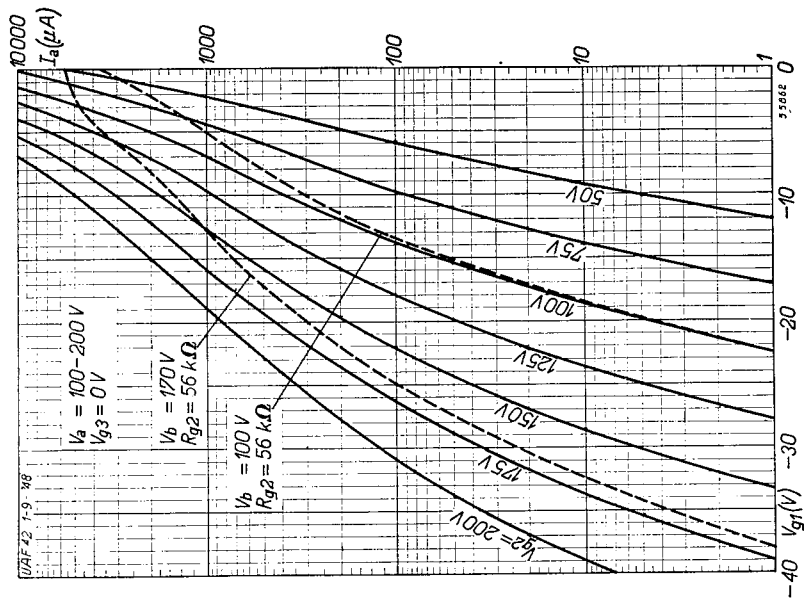


Fig. 8

Anode current ( $I_a$ , Fig. 8) and mutual conductance ( $S$ , Fig. 9) of the UAF 42 as functions of the grid bias ( $V_{g1}$ ) for various values of the screen grid voltage ( $V_{g2}$ ). The dotted lines indicate the variations in anode current and mutual conductance when a series resistor of  $56 k\Omega$  is included in the screen grid circuit.

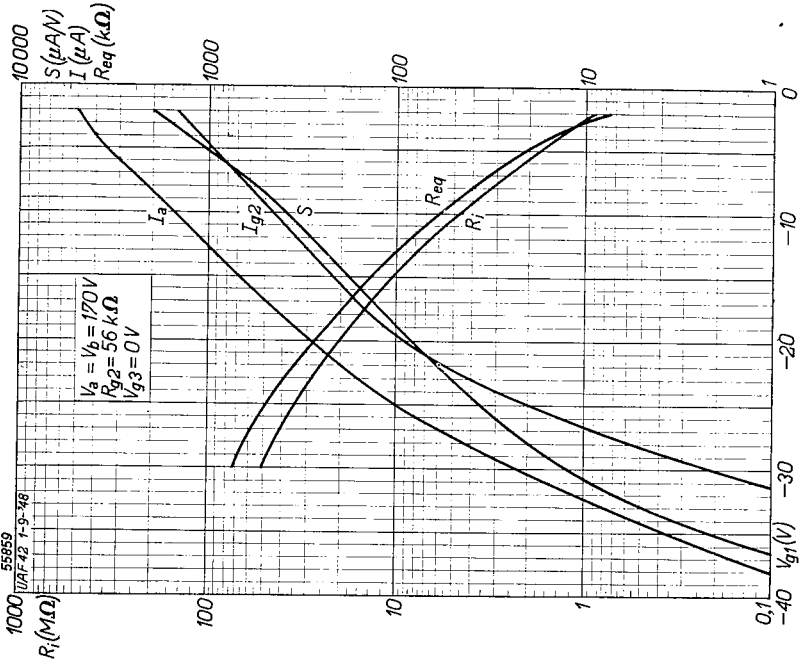


Fig. 11

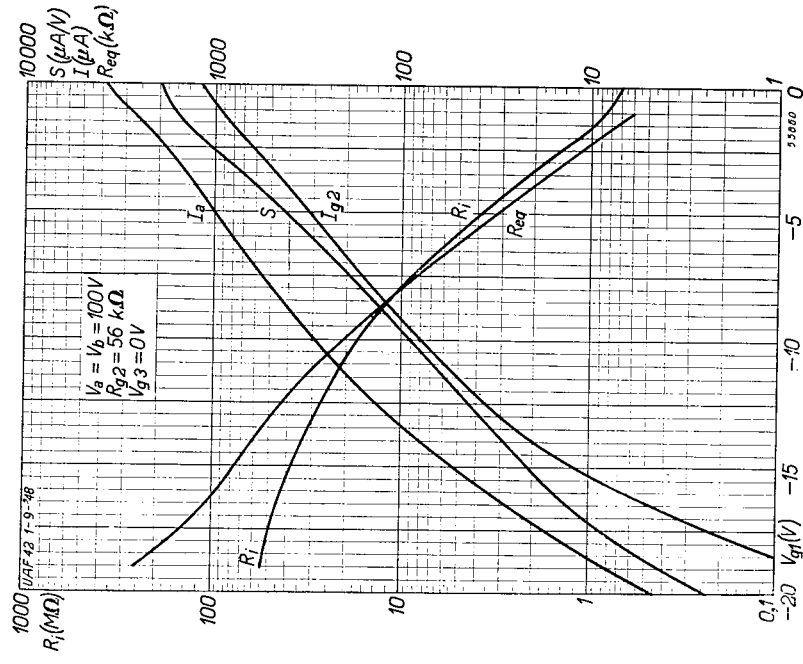


Fig. 10

Anode current ( $I_a$ ), screen grid current ( $I_{g2}$ ), mutual conductance ( $S$ ), internal resistance ( $R_i$ ) and equivalent noise resistance ( $R_{eq}$ ) of the pentode section of the UAF 42, as functions of the grid bias ( $V_{g1}$ ); screen grid resistor  $R_{g2} = 56 k\Omega$ , anode and supply voltage = 100 V (Fig. 10) and 170 V (Fig. 11).

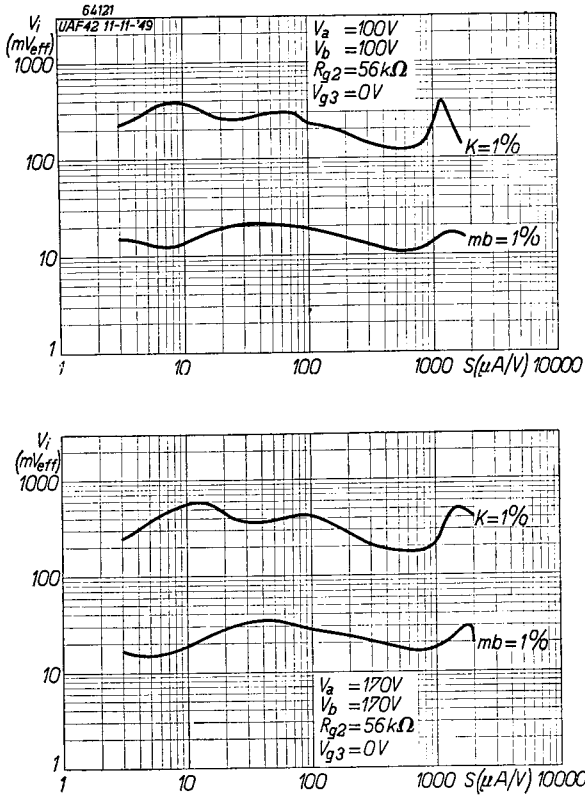


Fig. 12  
The effective voltage ( $V_i$ ) of an interfering R.F. signal on the control grid of the UAF 42, producing 1% cross-modulation; also that of an A.F. signal producing 1% modulation hum (curve  $m_b = 1\%$ ), both as a function of the mutual conductance ( $S$ ). Screen grid series resistor  $R_{g2} = 56 k\Omega$ , anode and supply voltage = 100 V (upper figure) and 170 V (lower figure).

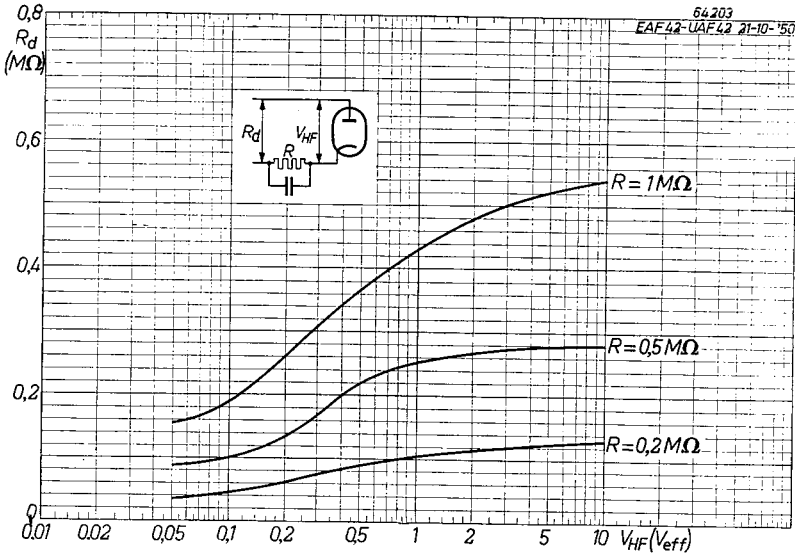


Fig. 13

Damping resistance of the diode of the UAF 42 as a function of the applied R.F. signal, for different values of the series resistor in the detector circuit. For detection characteristic of the diode see Fig. 7 in the description of the EBC 41.

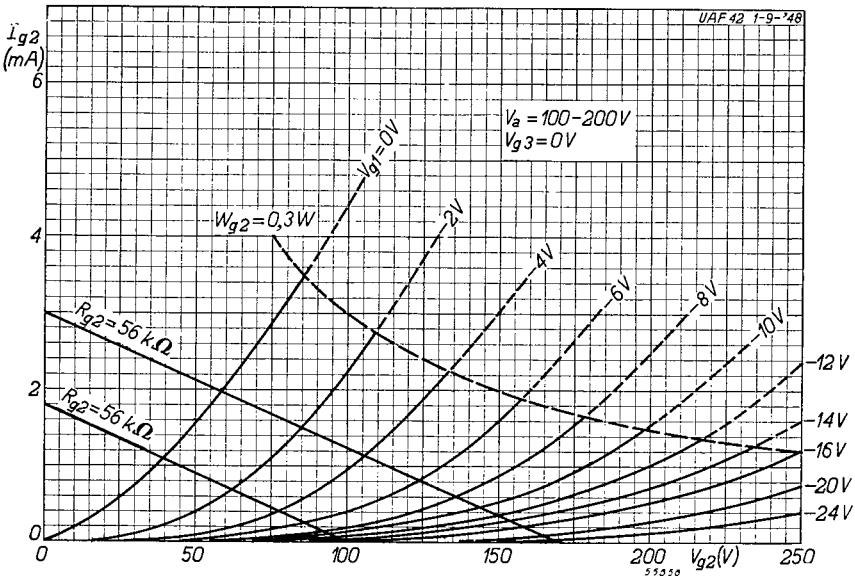


Fig. 14

Screen grid current ( $I_{g2}$ ) of the pentode section of the UAF 42 as a function of the screen grid voltage ( $V_{g2}$ ) with grid bias ( $V_{g1}$ ) as parameter. The maximum permissible screen grid dissipation (0.3 W) is indicated by the dotted line. The straight lines give the working characteristic for a screen grid series resistor of 56 k $\Omega$ , at supply voltages of 170 and 100 V.

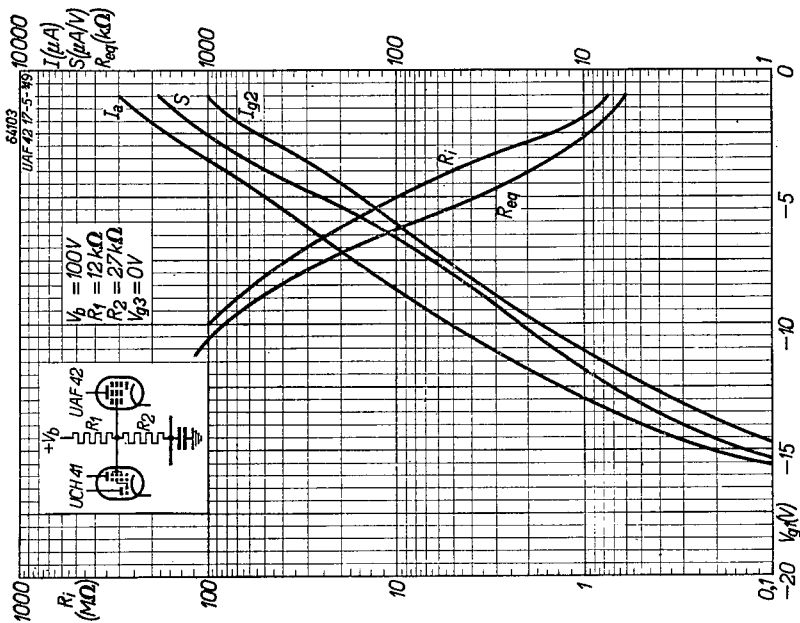


Fig. 15  
As Figs. 10 and 11, but with the screen grid voltage of the UAF 42 obtained by means of the same potentiometer as that of the frequency changer UCH 41.

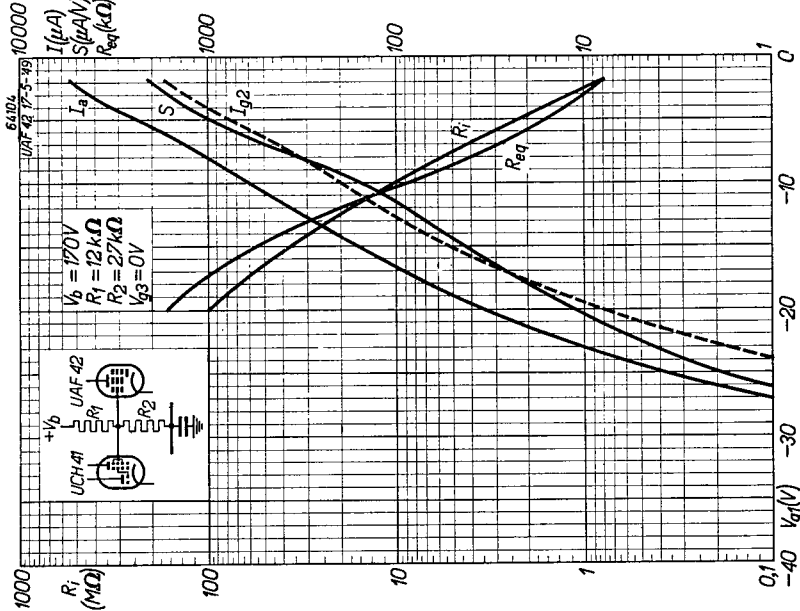


Fig. 16



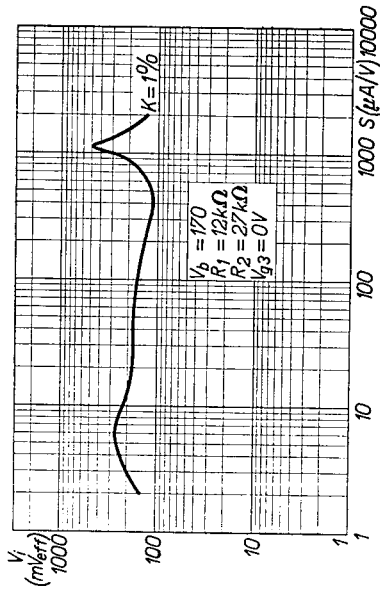
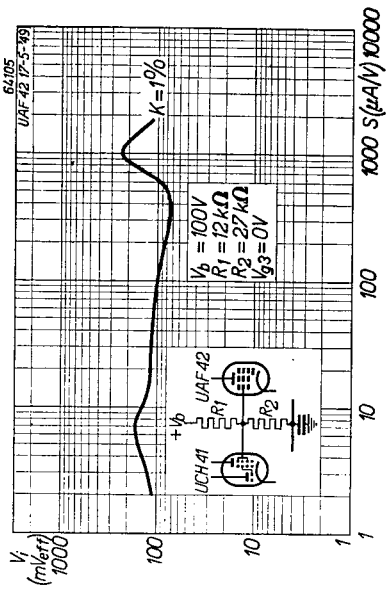


Fig. 17

As Fig. 12, but with the screen grids of the UAF 42 and UCH 41 fed by means of a common potentiometer.

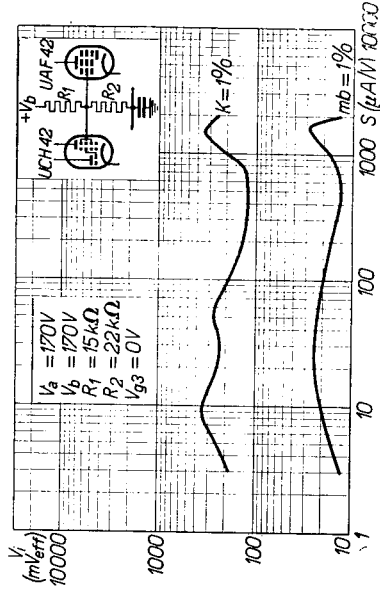
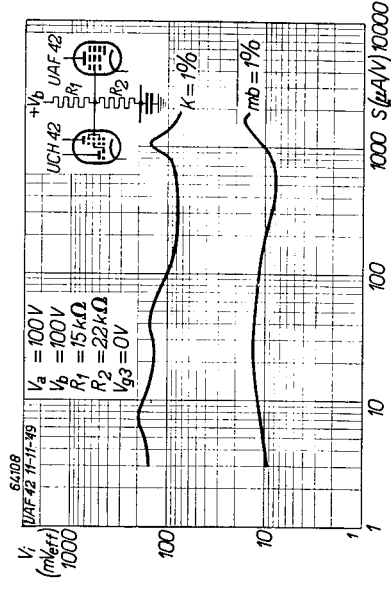


Fig. 18

As Fig. 12, but with the screen grids of the UAF 42 and UCH 42 fed by means of a common potentiometer.

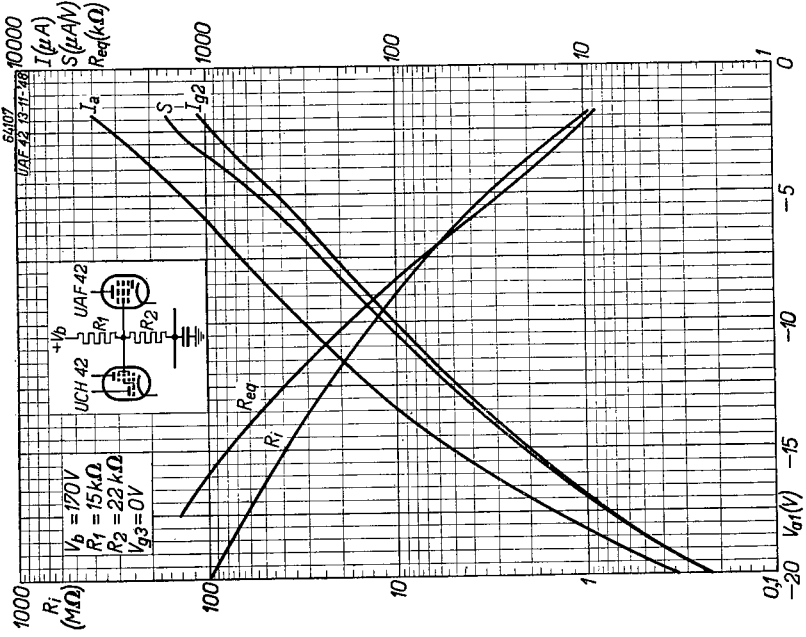


Fig. 19 As Figs. 10 and 11, but with the screen grid feeds of the UAF 42 and UCH 42 taken from a common potentiometer.

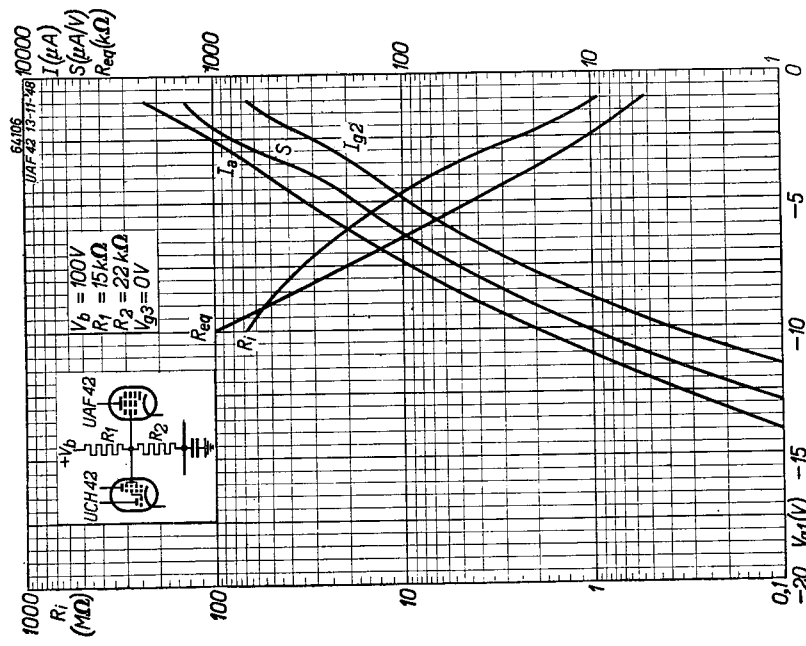


Fig. 20